

# Dynamical systems and Control

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# Lecture 7: Control

- Recap
- Feedback issues
- Systems that are difficult to control
- PID tuning for simple systems

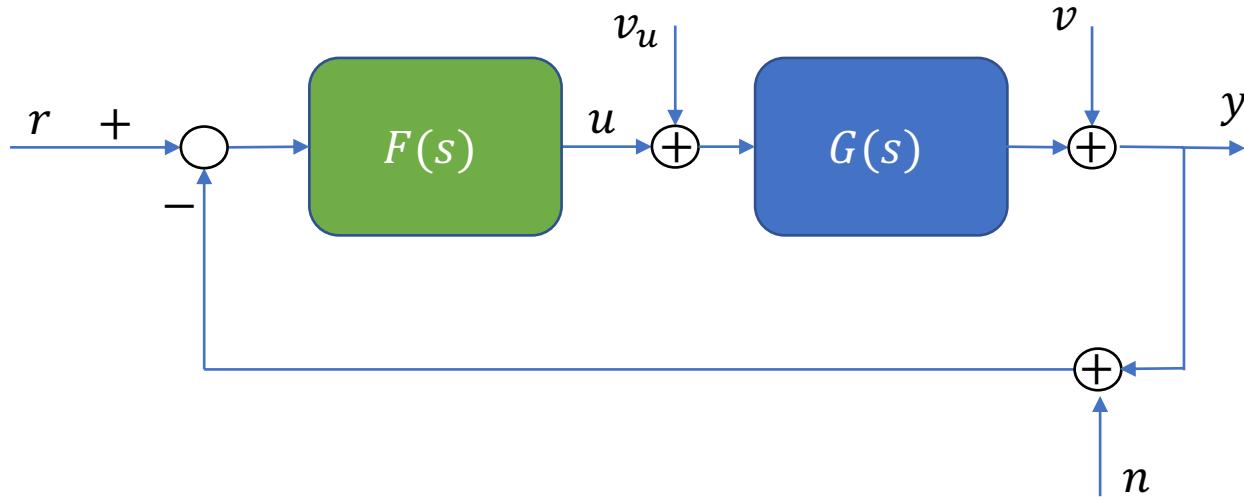
# PID controller

A quick recap of lecture 6

# Proportional-Integrator-Derivative (PID):

$$u(t) = K_P e(t) + K_I \int_0^t e(\tau) d\tau + K_D \dot{e}(t)$$

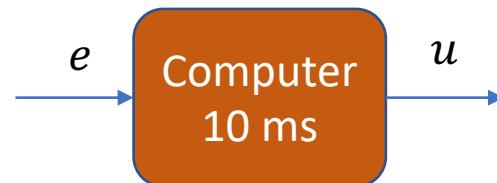
# Feedback issues



$$Y(s) = \frac{F(s)G(s)}{1 + F(s)G(s)}R(s) + \frac{G(s)}{1 + F(s)G(s)}V_u(s) + \frac{1}{1 + F(s)G(s)}V(s) - \frac{F(s)G(s)}{1 + F(s)G(s)}N(s)$$

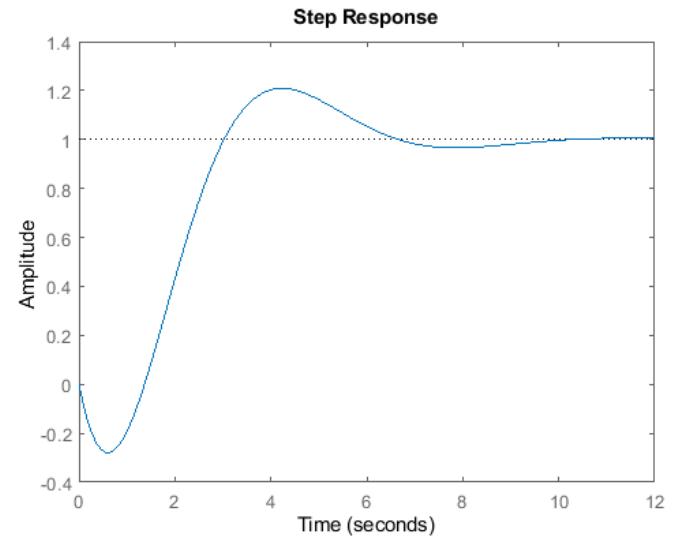
# Systems that are difficult to control

# Systems with time delay



# Systems with zero on RHS

The initial response can have undershoot.



# Unstable systems

We should stabilize the system.

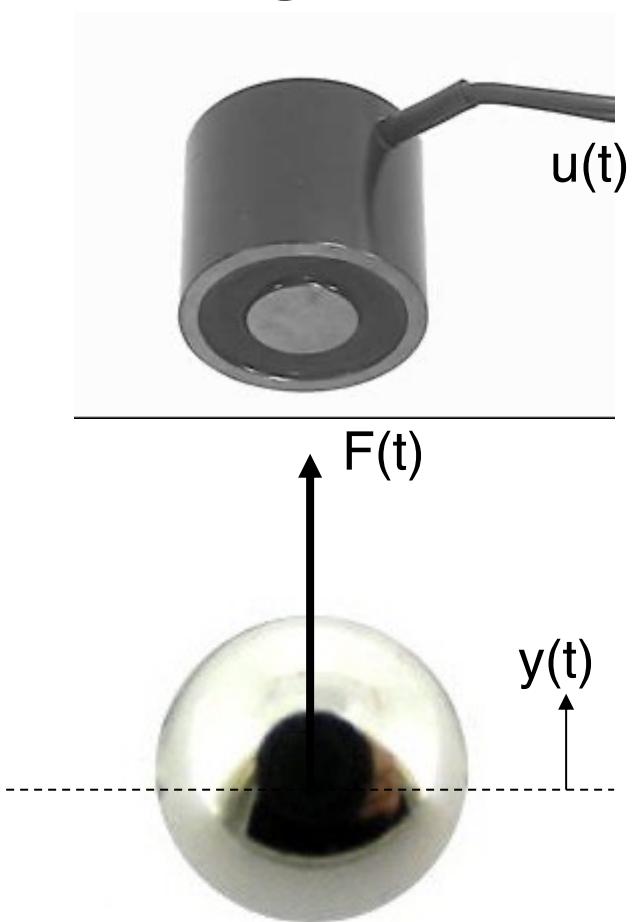
# Example-Controller design for floating ball

$y(t)$ : The position of the ball

$F(t)$ : Generated magnetic force

$u(t)$ : Voltage to the electromagnet

$$G(s) = \frac{1}{s^2 - 1}$$



# Example-Continued-P controller

P-controller:

$$F(s) = K_P$$

The system:

$$G(s) = \frac{1}{s^2 - 1}$$

# Example-Continued-P controller

P-controller:

$$F(s) = K_P$$

The system:

$$G(s) = \frac{1}{s^2 - 1}$$

The transfer function of the closed-loop system:

$$G_c(s) = \frac{F(s)G(s)}{1 + F(s)G(s)}$$

$$G_c = \frac{K_P / s^2 - 1}{1 + K_P / s^2 - 1} = \frac{K_P}{s^2 + K_P - 1}$$

Poles:  $\lambda = \pm\sqrt{1 - K_P}$

If  $1 - K_P > 0$ :  $\rightarrow$  Real and at least one positive

Always unstable!

If  $1 - K_P \leq 0$ :  $\rightarrow$  Complex with zero real part

# Example-Continued-PI controller

PI-controller:

$$F(s) = K_P + \frac{K_I}{s}$$

The system:

$$G(s) = \frac{1}{s^2 - 1}$$

# Example-Continued-PI controller

PI-controller:

$$F(s) = K_P + \frac{K_I}{s}$$

The system:

$$G(s) = \frac{1}{s^2 - 1}$$

The transfer function of the closed-loop system:

$$G_c(s) = \frac{F(s)G(s)}{1 + F(s)G(s)}$$

$$G_c = \frac{\left(K_P + \frac{K_I}{s}\right)\left(\frac{1}{s^2 - 1}\right)}{1 + \left(K_P + \frac{K_I}{s}\right)\left(\frac{1}{s^2 - 1}\right)} = \frac{K_P s + K_I}{s^3 + (K_P - 1)s + K_I}$$

First order:  $s + c$  stable if and only if  $c > 0$

Second order:  $s^2 + as + b$  stable if and only if  $a > 0, b > 0$

Third order:  $(s + c)(s^2 + as + b)$  if stable, then all coefficients should be positive

$s^2$  is missing so unstable!

# Example-Continued-PD controller

PD-controller:

$$F(s) = K_P + K_D s$$

The system:

$$G(s) = \frac{1}{s^2 - 1}$$

# Example-Continued-PD controller

PD-controller:

$$F(s) = K_P + K_D s$$

The system:

$$G(s) = \frac{1}{s^2 - 1}$$

The transfer function of the closed-loop system:

$$G_c(s) = \frac{F(s)G(s)}{1 + F(s)G(s)}$$

$$G_c = \frac{(K_P + K_D s)(\frac{1}{s^2 - 1})}{1 + (K_P + K_D s)(\frac{1}{s^2 - 1})} = \frac{K_P + K_D s}{s^2 + K_D s + K_P - 1}$$

Stable if  $K_D > 0, K_P > 1$

# PID tuning for simple systems

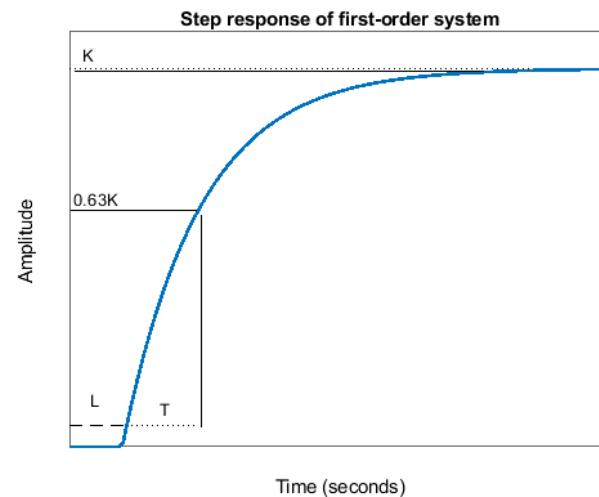
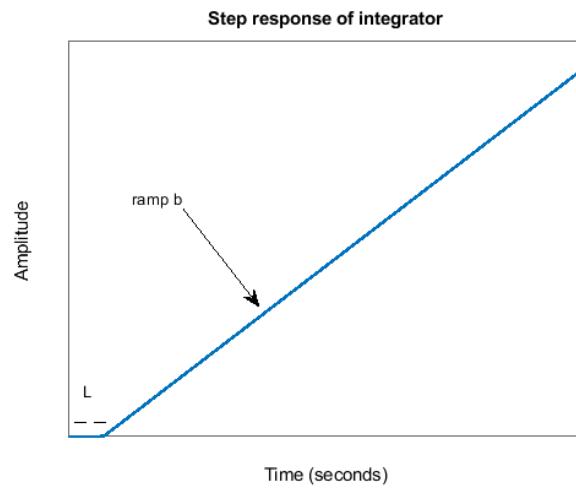
# How to tune PID?

- Trial and error: Experience
- Complete model + analysis of the poles
- Simplified model + tuning rules

# Simplified models are:

- Integrators
- First-order dynamics

# Study the step response



$$G(s) = \frac{b}{s} e^{-sL}$$

$$G(s) = \frac{K_{process}}{Ts + 1} e^{-sL}$$

# Ziegler-Nichols method for Integrators

- Calculate  $b$  and  $L$
- Select the gains according to the table on p. 44 in the complementary material

For example, for a P controller:  $K = \frac{1}{bL}$

Regulator	$K$	$T_i$	$T_d$
P	$1/(bL)$		
PI	$0.9/(bL)$	$3L$	
PID	$1.2/(bL)$	$2L$	$L/2$

# $\lambda$ -tunning for first-order systems

Define the desired closed loop system as

$$G_c = \frac{1}{sT_c + 1} e^{-Ls}$$

Let

$$\lambda = \frac{T_c}{T}$$

# $\lambda$ -tunning for first-order systems

$$G_c(s) = \frac{G(s)F(s)}{1 + G(s)F(s)} = \frac{1}{sT_c + 1} e^{-Ls}$$

# $\lambda$ -tunning for first-order systems

$$G_c(s) = \frac{G(s)F(s)}{1 + G(s)F(s)} = \frac{1}{sT_c + 1} e^{-Ls}$$

From the above equation, we obtain:

$$F(s) = \frac{G_c(s)}{G(s)(1 - G_c(s))}$$

Now, replace  $G_c(s) = \frac{1}{sT_c + 1} e^{-Ls}$  and  $G(s) = \frac{K_{process}}{Ts + 1} e^{-sL}$

$$\begin{aligned} F(s) &= \frac{\frac{e^{-Ls}}{sT_c + 1}}{\frac{K_{process}}{Ts + 1} e^{-sL} \left(1 - \frac{e^{-Ls}}{sT_c + 1}\right)} = \frac{Ts + 1}{K_{process}(sT_c + 1 - e^{-Ls})} \approx \frac{Ts + 1}{K_{process}(sT_c + 1 - 1 + Ls)} \\ &= \frac{s + 1/T}{K_{process}(s\lambda + Ls)} = \frac{T}{K_{process}(\lambda T + L)} \frac{s + 1/T_c}{s} = \frac{T}{K_{process}(\lambda T + L)} \left(1 + \frac{1}{TS}\right) \end{aligned}$$

A PI controller!

$$K_P = \frac{T}{K_{process}(\lambda T + L)}$$

$$K_I = \frac{1}{K_{process}(\lambda T + L)}$$

# What do we cover next?

- PID discretization
- Integral windup
- Derivative filtering

# Ask us!

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