## Examination TSTE25

Date:
Time:
Tentajour:
Permitted aids: A sheet of paper with formulae and a scientific calculator.

Exercise 1. A power transmission company has been tasked with building a 600 kV 5000 MW HVDC link between Stavanger, Norway to Fraserburgh, Scotland. A key component in the HVDC link is the power converter. What is the type and rating of semiconductor switches should they consider for the converter? Motivate.
(2 point)
Exercise 2. Consider all components to be ideal in a step-down converter used in a small portable PV phone charger and let the average output voltage $\left(V_{o}\right)$ be held constant at 5 V . If input voltage $\left(V_{i}\right)$ is $10-40 \mathrm{~V}$, output power, $P_{o} \geq 15 \mathrm{~W}$, and switching frequency, $f_{s}=50 \mathrm{kHz}$, calculate the following:
a) The switch duty ratio $(D)$ that is required to maintain the average output voltage of 5 V .
(1 point)
b) The minimum inductance $(L)$ required to keep the converter operation in a continuous-conduction mode under all conditions.
(4 point)
c) The minimum capacitance $(C)$ required to keep the output peak-to-peak ripple to be $10 \%$ of the average output voltage.
(2 point)
d) The minimum efficiency of the DC-DC converter. IRF540 MOSFETs are employed (datasheet found at the end of the document) and the voltage and current switching transient times are (4 point)

$$
t_{r i}=19 \mathrm{~ns}, \quad t_{f v}=34 \mathrm{~ns}, \quad t_{r v}=12 \mathrm{~ns}, \quad t_{f i}=16 \mathrm{~ns}
$$

Exercise 3. Consider all components to be ideal in a step-up converter used in a power management system in a vehicle and let the average output voltage $\left(V_{o}\right)$ be held constant at 5 V . If battery voltage on the input side $\left(V_{i}\right)$ is $2.9-4.2 \mathrm{~V}, P_{o} \geq 200 \mathrm{~W}$, and due to cost limitations, the only available passive components are an inductor, $L=10 \mu \mathrm{H}$, and several capacitors of $100 \mu \mathrm{~F}$. Calculate the following:
a) The switch duty ratio $(D)$ that is required to maintain the average output voltage of 5 V .
(1 point)
b) The minimum switching frequency $\left(f_{s}\right)$ required to keep the battery current peak-to-peak ripple below $10 \%$ of the average battery current.
(4 point)
c) The minimum number of capacitors required to keep the output peak-to-peak voltage ripple below $10 \%$ of the average output voltage.
(3 point)

Exercise 4. For a half-bridge inverter, assuming all ideal components, the output waveforms are presented in Figure 1, where

> peak inverter side voltage peak inverter side voltage (fundamental) peak output current peak output voltage peak output voltage (fundamental)

$$
\begin{aligned}
\hat{v}_{s} & =12 \mathrm{~V}, \\
\hat{v}_{s(1)} & =9.61 \mathrm{~V}, \\
\hat{i}_{\text {out }} & =40.1 \mathrm{~A}, \\
\hat{v}_{\text {out }} & =11 \mathrm{~V}, \\
\hat{v}_{\text {out }(1)} & =8.37 \mathrm{~V} .
\end{aligned}
$$

Determine:
a) The switching frequency used
b) The inductance
c) The peak fundamental current
d) The pole-to-pole DC-link voltage $\left(V_{d}\right)$ and modulation index $\left(m_{a}\right)$
e) The active power on the load at the fundamental frequency.
f) The phase angle of the fundamental current with respect to the inverter side voltage. (2 point)
g) The active and reactive power on the converter at the fundamental frequency.


Figur 1: half-bridge inverter output waveforms.

Exercise 5. Consider the switched step-down converter shown in Figure 2. The drain current of the MOSFET as a function through one complete turn-on and turn-off sequence is shown in Figure 2. The switch $\left(S_{W}\right)$ and diode $\left(D_{f}\right)$ data are provided in Table 1.


Figur 2: Switched step-down converter and drain current transients.

Tabell 1: switch $\left(S_{W}\right)$ and diode $\left(D_{f}\right)$ data.

| $S_{W}$ data |  | $D_{f}$ data |  |
| :---: | :---: | :---: | :---: |
| $V_{d s(\max )}$ | 700 V | $V_{r m}$ | 800 V |
| $I_{d(\max )}$ | 400 V | $I_{\max }$ | 400 A |
| $T_{j(\max )}$ | $150^{\circ} \mathrm{C}$ | $T_{j(\max )}$ | $150^{\circ} \mathrm{C}$ |
| $R_{\theta(\mathrm{ja})}$ | $0.1^{\circ} \mathrm{C} / \mathrm{W}$ | $R_{\theta(\mathrm{ja})}$ | $1^{\circ} \mathrm{C} / \mathrm{W}$ |
| $R_{\text {on }}$ | $0.01 \Omega$ | $R_{\text {on }}$ | $0.1 \Omega$ |
|  |  | $V_{\text {on }}$ | 0.7 V |

a) Sketch and dimension the drain-source voltage of $S_{W}$ as a function of time. Assume that the voltage across the switch can change instantaneously and is only limited by the external circuit.
b) Sketch and dimension the diode voltage as a function of time.
c) Are either the diode or the switch overstressed with respect to voltage? If so, specify by how much.
d) Determine the junction temperature of the switch and the diode. Do not forget the losses during the switching transients, the diode reverse recovery, a duty cycle of $90 \%$, and assuming a switching frequency of 10 kHz at an ambient temperature of $25^{\circ} \mathrm{C}$.
(6 point)
Exercise 6. Consider the problem of ripple in the output current of a single-phase full-bridge inverter. Assume $V_{o(1)}=200 \mathrm{~V}$ and $I_{o(1)}=10 \mathrm{~A}$ at a frequency of 50 Hz and an induction motor load with inductance of $\mathrm{L}=10 \mathrm{mH}$. Calculate the peak value of the inverter ripple current if the converter is operating in a sinusoidal unipolar PWM mode, with $m_{f}=21$ and $m_{a}=0.8$. ( 8 point)

Tabell 2: Generalized harmonics of a half-bridge inverter output voltage for a large $m_{f}$.

| $h \downarrow \quad m_{a} \rightarrow$ | 0.2 | 0.4 | 0.6 | 0.8 | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0.2 | 0.4 | 0.6 | 0.8 | 1 |
| Fundamental |  |  |  |  |  |
| $m_{f}$ | 1.242 | 1.15 | 1.006 | 0.818 | 0.6023 |
| $m_{f} \pm 2$ | 0.061 | 0.061 | 0.131 | 0.22 | 0.318 |
| $m_{f} \pm 4$ |  |  |  |  | 0.018 |
| $2 m_{f} \pm 1$ | 0.19 | 0.326 | 0.37 | 0.314 | 0.181 |
| $2 m_{f} \pm 3$ |  | 0.024 | 0.071 | 0.139 | 0.212 |
| $2 m_{f} \pm 5$ |  |  |  | 0.013 | 0.033 |
| $3 m_{f}$ | 0.335 | 0.123 | 0.083 | 0.171 | 0.133 |
| $3 m_{f} \pm 2$ | 0.044 | 0.139 | 0.203 | 0.176 | 0.062 |
| $3 m_{f} \pm 4$ |  | 0.012 | 0.047 | 0.104 | 0.157 |
| $3 m_{f} \pm 6$ |  |  |  | 0.016 | 0.044 |
| $4 m_{f} \pm 1$ | 0.163 | 0.157 | 0.088 | 0.105 | 0.068 |
| $4 m_{f} \pm 3$ | 0.012 | 0.070 | 0.132 | 0.115 | 0.009 |
| $4 m_{f} \pm 5$ |  |  | 0.034 | 0.084 | 0.119 |
| $4 m_{f} \pm 7$ |  |  |  | 0.017 | 0.05 |

Note: output voltage $\left(\hat{V}_{o}\right)$ is $\hat{V}_{o}=m_{a} V_{d} / 2$.

## Power MOSFET



## FEATURES

- Dynamic dV/dt Rating
- Repetitive Avalanche Rated
- $175{ }^{\circ} \mathrm{C}$ Operating Temperature
- Fast Switching
- Ease of Paralleling
- Simple Drive Requirements
- Lead (Pb)-free Available


## DESCRIPTION

Third generation Power MOSFETs from Vishay provide the designer with the best combination of fast switching, ruggedized device design, low on-resistance and cost-effectiveness.
The TO-220 package is universally preferred for all commercial-industrial applications at power dissipation levels to approximately 50 W . The low thermal resistance and low package cost of the TO-220 contribute to its wide acceptance throughout the industry

## ORDERING INFORMATION

| Package | TO-220 |
| :--- | :--- |
| Lead (Pb)-free | IRF540PbF |
|  | SiHF540-E3 |
| SnPb | IRF540 |
|  | SiHF540 |


| ABSOLUTE MAXIMUM RATINGS $\mathrm{T}_{\mathrm{C}}=25^{\circ} \mathrm{C}$, unless otherwise noted |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| PARAMETER |  |  | SYMBOL | LIMIT | UNIT |
| Drain-Source Voltage |  |  | $\mathrm{V}_{\text {DS }}$ | 100 | V |
| Gate-Source Voltage |  |  | $\mathrm{V}_{\mathrm{GS}}$ | $\pm 20$ |  |
| Continuous Drain Current | $\mathrm{V}_{\mathrm{GS}}$ at 10 V | $\mathrm{T}_{\mathrm{C}}=25^{\circ} \mathrm{C}$ | ID | 28 | A |
|  |  | $\mathrm{T}_{\mathrm{C}}=100^{\circ} \mathrm{C}$ |  | 20 |  |
| Pulsed Drain Current ${ }^{\text {a }}$ |  |  | $\mathrm{I}_{\mathrm{DM}}$ | 110 |  |
| Linear Derating Factor |  |  |  | 1.0 | W/ ${ }^{\circ} \mathrm{C}$ |
| Single Pulse Avalanche Energy ${ }^{\text {b }}$ |  |  | $\mathrm{E}_{\text {AS }}$ | 230 | mJ |
| Repetitive Avalanche Current ${ }^{\text {a }}$ |  |  | $\mathrm{I}_{\text {AR }}$ | 28 | A |
| Repetitive Avalanche Energy ${ }^{\text {a }}$ |  |  | $\mathrm{E}_{\text {AR }}$ | 15 | mJ |
| Maximum Power Dissipation | $\mathrm{T}_{\mathrm{C}}=25^{\circ} \mathrm{C}$ |  | PD | 150 | W |
| Peak Diode Recovery dV/dtc |  |  | dV/dt | 5.5 | V/ns |
| Operating Junction and Storage Temperature Range |  |  | $\mathrm{T}_{\mathrm{J}}, \mathrm{T}_{\text {stg }}$ | -55 to +175 | ${ }^{\circ} \mathrm{C}$ |
| Soldering Recommendations (Peak Temperature) | for 10 s |  |  | $300{ }^{\text {d }}$ |  |
| Mounting Torque | 6-32 or M3 screw |  |  | 10 | $\mathrm{lbf} \cdot \mathrm{in}$ |
|  |  |  |  | 1.1 | $\mathrm{N} \cdot \mathrm{m}$ |

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. Repetitive rating; pulse width limited by maximum junction temperature (see fig. 11).
b. $V_{D D}=25 \mathrm{~V}$, starting $T_{J}=25^{\circ} \mathrm{C}, \mathrm{L}=440 \mu \mathrm{H}, \mathrm{R}_{\mathrm{G}}=25 \Omega, \mathrm{I}_{\mathrm{AS}}=28 \mathrm{~A}$ (see fig. 12).
c. $I_{\mathrm{SD}} \leq 28 \mathrm{~A}, \mathrm{dl} / \mathrm{dt} \leq 170 \mathrm{~A} / \mu \mathrm{s}, \mathrm{V}_{\mathrm{DD}} \leq \mathrm{V}_{\mathrm{DS}}, \mathrm{T}_{\mathrm{J}} \leq 175^{\circ} \mathrm{C}$.
d. 1.6 mm from case

* Pb containing terminations are not RoHS compliant, exemptions may apply

| THERMAL RESISTANCE RATINGS |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| PARAMETER | SYMBOL | TYP. | MAX. | UNIT |
| Maximum Junction-to-Ambient | $\mathrm{R}_{\text {thJA }}$ | - | 62 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| Case-to-Sink, Flat, Greased Surface | $\mathrm{R}_{\text {thcs }}$ | 0.50 | - |  |
| Maximum Junction-to-Case (Drain) | $\mathrm{R}_{\text {thJC }}$ | - | 1.0 |  |


| SPECIFICATIONS $\mathrm{T}_{J}=25^{\circ} \mathrm{C}$, unless otherwise noted |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PARAMETER | SYMBOL | TEST CONDITIONS |  | MIN. | TYP. | MAX. | UNIT |
| Static |  |  |  |  |  |  |  |
| Drain-Source Breakdown Voltage | $\mathrm{V}_{\mathrm{DS}}$ | $\mathrm{V}_{\mathrm{GS}}=0 \mathrm{~V}, \mathrm{I}_{\mathrm{D}}=250 \mu \mathrm{~A}$ |  | 100 | - | - | V |
| $\mathrm{V}_{\mathrm{DS}}$ Temperature Coefficient | $\Delta \mathrm{V}_{\mathrm{DS}} / \mathrm{T}_{\mathrm{J}}$ | Reference to $25^{\circ} \mathrm{C}, \mathrm{I}_{\mathrm{D}}=1 \mathrm{~mA}$ |  | - | 0.13 | - | V/ ${ }^{\circ} \mathrm{C}$ |
| Gate-Source Threshold Voltage | $\mathrm{V}_{\mathrm{GS} \text { (th) }}$ | $\mathrm{V}_{\mathrm{DS}}=\mathrm{V}_{\mathrm{GS}}, \mathrm{I}_{\mathrm{D}}=250 \mu \mathrm{~A}$ |  | 2.0 | - | 4.0 | V |
| Gate-Source Leakage | IGss | $\mathrm{V}_{\mathrm{GS}}= \pm 20 \mathrm{~V}$ |  | - | - | $\pm 100$ | nA |
| Zero Gate Voltage Drain Current | Idss | $\mathrm{V}_{\mathrm{DS}}=100 \mathrm{~V}, \mathrm{~V}_{\mathrm{GS}}=0 \mathrm{~V}$ |  | - | - | 25 | $\mu \mathrm{A}$ |
|  |  | $\mathrm{V}_{\mathrm{DS}}=80 \mathrm{~V}, \mathrm{~V}_{\mathrm{GS}}=0 \mathrm{~V}, \mathrm{~T}_{\mathrm{J}}=150{ }^{\circ} \mathrm{C}$ |  | - | - | 250 |  |
| Drain-Source On-State Resistance | $\mathrm{R}_{\mathrm{DS} \text { (on) }}$ | $\mathrm{V}_{\mathrm{GS}}=10 \mathrm{~V}$ | $\mathrm{I}_{\mathrm{D}}=17 \mathrm{~A}^{\mathrm{b}}$ | - | - | 0.077 | $\Omega$ |
| Forward Transconductance | $\mathrm{g}_{\mathrm{fs}}$ | $\mathrm{V}_{\mathrm{DS}}=50 \mathrm{~V}, \mathrm{I}_{\mathrm{D}}=17 \mathrm{Ab}$ |  | 8.7 | - | - | S |
| Dynamic |  |  |  |  |  |  |  |
| Input Capacitance <br> Output Capacitance |  | $\begin{gathered} \mathrm{V}_{\mathrm{GS}}=0 \mathrm{~V}, \\ \mathrm{~V}_{\mathrm{DS}}=25 \mathrm{~V}, \\ \mathrm{f}=1.0 \mathrm{MHz}, \text { see fig. } 5 \end{gathered}$ |  | - | 1700 | - | pF |
|  | $\mathrm{C}_{\text {oss }}$ |  |  | - | 560 | - |  |
| Reverse Transfer Capacitance | $\mathrm{C}_{\text {rss }}$ |  |  | - | 120 | - |  |
| Total Gate Charge | $\mathrm{Q}_{\mathrm{g}}$ | $\mathrm{V}_{\mathrm{GS}}=10 \mathrm{~V}$ | $\begin{gathered} I_{D}=17 \mathrm{~A}, V_{D S}=80 \mathrm{~V}, \\ \text { see fig. } 6 \text { and } 13^{b} \end{gathered}$ | - | - | 72 | nC |
| Gate-Source Charge | $\mathrm{Q}_{\mathrm{gs}}$ |  |  | - | - | 11 |  |
| Gate-Drain Charge | $\mathrm{Q}_{\mathrm{gd}}$ |  |  | - | - | 32 |  |
| Turn-On Delay Time | $\mathrm{t}_{\mathrm{d}(\mathrm{on})}$ | $\begin{gathered} V_{D D}=50 \mathrm{~V}, \mathrm{I}_{\mathrm{D}}=17 \mathrm{~A} \\ \mathrm{R}_{\mathrm{G}}=9.1 \Omega, R_{D}=2.9 \Omega \text {, see fig. } 10^{\mathrm{b}} \end{gathered}$ |  | - | 11 | - | ns |
| Rise Time | $\mathrm{t}_{\mathrm{r}}$ |  |  | - | 44 |  |  |
| Turn-Off Delay Time | $\mathrm{t}_{\mathrm{d} \text { (off) }}$ |  |  | - | 53 | - |  |
| Fall Time | $\mathrm{t}_{\mathrm{f}}$ |  |  | - | 43 | - |  |
| Internal Drain Inductance | $L_{D}$ | Between lead, 6 mm ( 0.25 ") from package and center of die contact |  | - | 4.5 | - | nH |
| Internal Source Inductance | Ls |  |  | - | 7.5 | - |  |
| Drain-Source Body Diode Characteristics |  |  |  |  |  |  |  |
| Continuous Source-Drain Diode Current | $I_{s}$ | MOSFET symbol showing the integral reverse p - n junction diode |  | - | - | 28 | A |
| Pulsed Diode Forward Current ${ }^{\text {a }}$ | ISM |  |  | - | - | 110 |  |
| Body Diode Voltage | $\mathrm{V}_{\text {SD }}$ | $\mathrm{T}_{\mathrm{J}}=25^{\circ} \mathrm{C}, \mathrm{I}_{\mathrm{S}}=28 \mathrm{~A}, \mathrm{~V}_{\mathrm{GS}}=0 \mathrm{~V}^{\mathrm{b}}$ |  | - | - | 2.5 | V |
| Body Diode Reverse Recovery Time | $\mathrm{t}_{\mathrm{rr}}$ | $\mathrm{T}_{J}=25^{\circ} \mathrm{C}, \mathrm{I}_{\mathrm{F}}=17 \mathrm{~A}, \mathrm{dl} / \mathrm{dt}=100 \mathrm{~A} / \mu \mathrm{s}^{\mathrm{b}}$ |  | - | 180 | 360 | ns |
| Body Diode Reverse Recovery Charge | $\mathrm{Q}_{\text {rr }}$ |  |  | - | 1.3 | 2.8 | $\mu \mathrm{C}$ |
| Forward Turn-On Time | $\mathrm{t}_{\text {on }}$ | Intrinsic turn-on time is negligible (turn-on is dominated by $L_{S}$ and $L_{D}$ ) |  |  |  |  |  |
| Notes <br> Repetitive rating; pulse width limited by Pulse width $\leq 300 \mu$ s; duty cycle $\leq 2 \%$. | imum junctio | emperature (see | 11). |  |  |  |  |

