

## Modellering

Ekvivalent enfaskrets för en trefasmotor matad med balanserad trefasström.

## Sammantänkligt flöde

Betrakta en statorlindning där energiomv. sker:

$$\lambda_a = L_{aa} i_a + L_{ab} i_b + L_{ac} i_c + L_{af} i_f \quad (1)$$

## Induktanser

• ömsinduktans mellan rotor och stator

$$L_{af} = L_{af} \cos \theta_{me} \quad (2)$$

• statorlindningarnas induktanser

$$L_{aa} = L_{bb} = L_{cc} = L_{aa} = L_{aa0} + L_{al} \quad (3)$$

↑  
 ges av luftgaps-  
 flödet

↑  
 ges av läckflödet

$$L_{ab} = L_{bc} = L_{ca} = L_{aa0} \cos\left(\frac{2\pi}{3}\right) = -\frac{1}{2} L_{aa0} \quad (4)$$

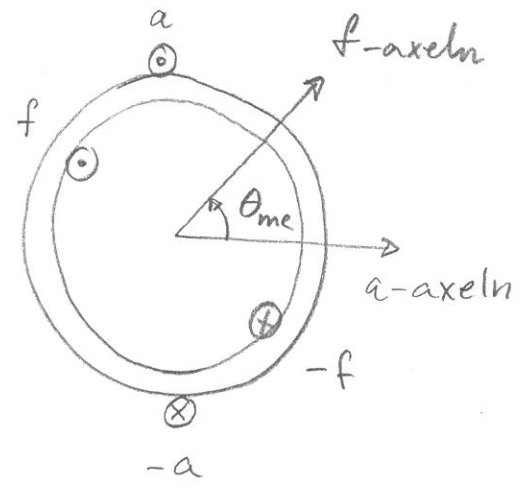
(2)-(4) i (1):

$$\begin{aligned}
 \lambda_a &= (L_{aa0} + L_{al}) i_a - \frac{1}{2} L_{aa0} i_b - \frac{1}{2} L_{aa0} i_c + L_{af} i_f = \\
 &= \underbrace{\left(\frac{3}{2} L_{aa0} + L_{al}\right)}_{=: \text{synkroninduktansen } L_s} i_a - \frac{1}{2} L_{aa0} \underbrace{(i_a + i_b + i_c)}_{=0} + L_{af} i_f \cos \theta_{me} \quad (5)
 \end{aligned}$$

# Krettsamband

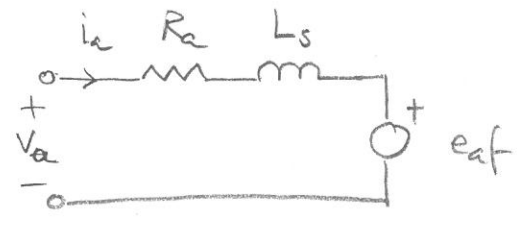
Låt:

- $i_a = \sqrt{2} I_a \cos \omega_e t$ ,  $i_f = \bar{I}_f$
- f-axeln ligger  $\delta_{e0}$  elektriska radianer före statorvägens magn. axel, dvs



$$\theta_{me} = \omega_e t + \delta_{e0}$$

## Statorkrets



$$V_a = R_a i_a + \frac{d\lambda_a}{dt} \quad (5)$$

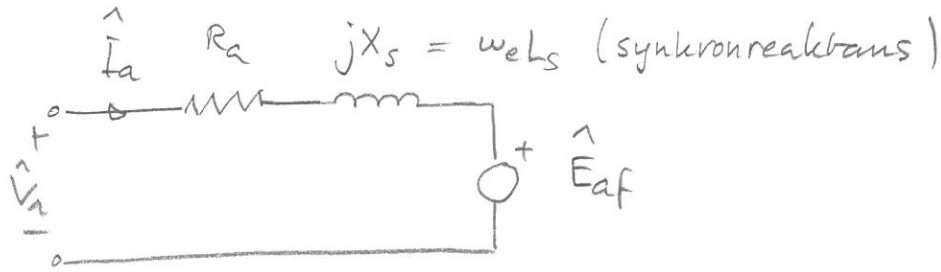
$$= R_a i_a + L_s \frac{di_a}{dt} + \frac{d}{dt} L_{af} I_f \cos(\omega_e t + \delta_{e0}) \Rightarrow$$

$$= -\omega_e L_{af} I_f \sin(\omega_e t + \delta_{e0}) =: e_{af}$$

$$V_a = R_a i_a + L_s \frac{di_a}{dt} + e_{af} \quad (6)$$

sinusvågor med vinkelhastighet  $\omega_e \Rightarrow$   
 jw-metoden kan användas!

# Komplex representation



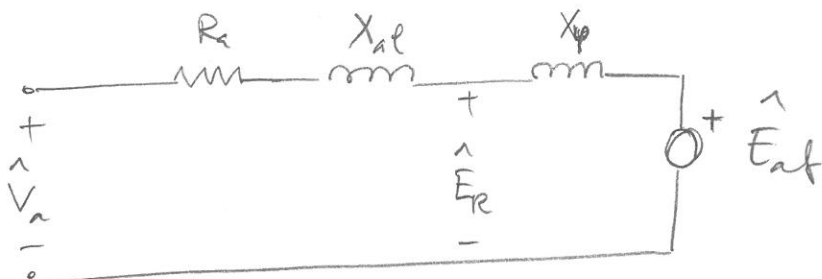
$$\hat{V}_a = R_a \hat{I}_a + jX_s \hat{I}_a + \hat{E}_{af} \quad (7)$$

$\hat{E}_{af}$  :    Låt  $i_a = \sqrt{2} \hat{I}_a \cos(\omega_e t)$  vara riktfas, dvs  
 $\hat{I}_a = \hat{I}_a$

$$\begin{aligned} e_{af} &= -\omega_e L_{af} I_f \sin(\omega_e t + \delta_{e0}) = /-\sin\alpha = \cos(\alpha + \frac{\pi}{2}) \\ &= \omega_e L_{af} I_f \cos(\omega_e t + \frac{\pi}{2} + \delta_{e0}) \Rightarrow \\ \hat{E}_{af} &= \frac{\omega_e L_{af} I_f}{\sqrt{2}} \cdot e^{j(\frac{\pi}{2} + \delta_{e0})} = j \cdot \frac{\omega_e L_{af} I_f}{\sqrt{2}} e^{j\delta_{e0}} \quad (8) \end{aligned}$$

Ibland delas  $X_s = \omega_e (\frac{3}{2} L_{aa0} + L_{al})$  upp i

- $X_p = \frac{3}{2} L_{aa0} \omega_e =$  magnetiseringsreaktansen
- $X_{al} = L_{al} \omega_e =$  läckreaktansen

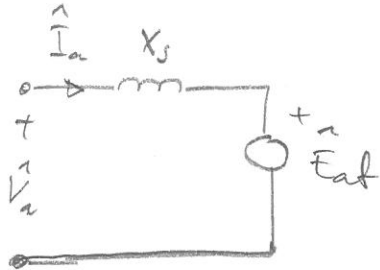


$\hat{E}_R$  = luftgapsspänningen = den inducerade spänningen av det totala luftgapsflödet från rotor + stator

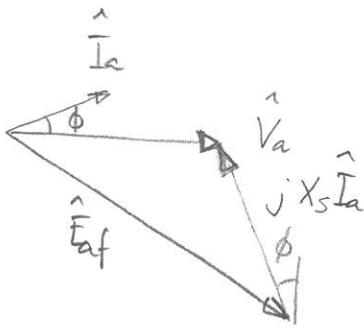
# Driftfall

Antag att  $R_a \approx 0 \Omega$ .

## Motordrift

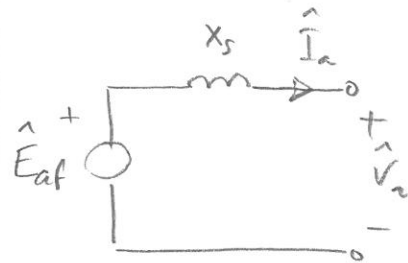


## Visardiagram

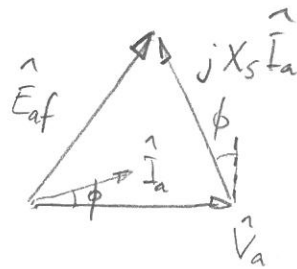


$\hat{V}_a$  är före  $\hat{E}_{af}$

## Generatordrift



## Visardiagram



$\hat{E}_{af}$  före  $\hat{V}_a$

# Parameterisering

$$\hat{V}_a = R_a \hat{I}_a + j X_s \hat{I}_a + \hat{E}_{af}$$

där  $X_s = \omega_e L_s$

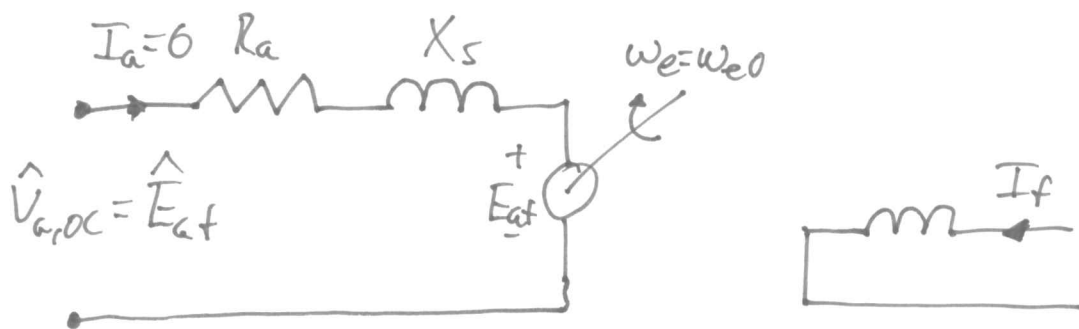
$$\hat{E}_{af} = j \left( \frac{\omega_e L_{af} I_f}{\sqrt{2}} \right) e^{j\delta_{e0}}$$

## Parametrar

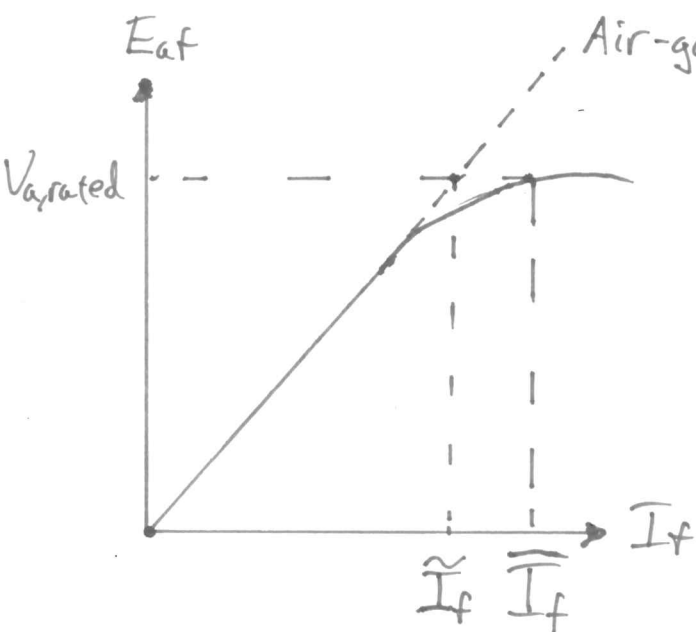
$$R_a, X_s, L_{af} \quad (L_s)$$

•  $R_a$  kan mätas

•  $L_{af}$ : Tomgångsprov (mättningskaraktäristik)



## Synkronmotorns magnetiseringskurva

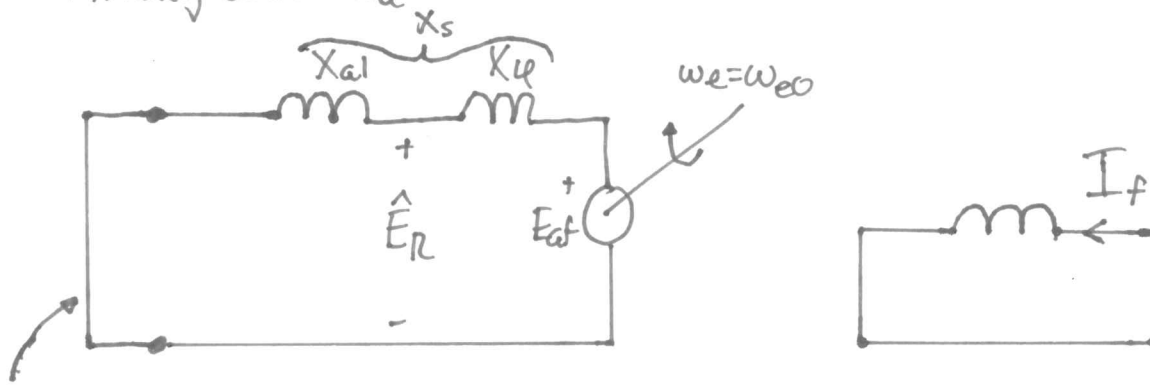


$$L_{af} = \frac{\sqrt{2} E_{af}}{\omega_{e0} I_f}$$

Notera:  $L_{af}$  minskar vid mätning

•  $L_s$ : Belastningsprov (kortsletnings karaktäristik) (scc) <sup>⑥</sup>

• Antag att  $R_a \approx 0$

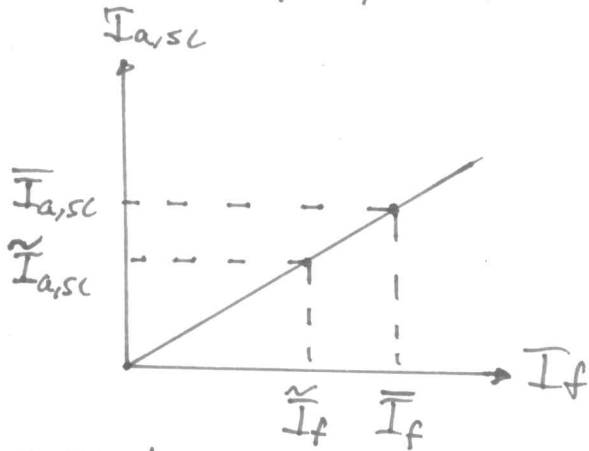


Kortslut alla faser.

$$\hat{E}_{af} = j X_s \hat{I}_{a,sc} \Rightarrow X_s = \frac{E_{af}}{I_{a,sc}}$$

Motor omätnad ty:

$B \sim E_R$ ,  $E_R \ll E_{af}$  ty  $X_{al} \ll X_\phi$



Omätnad synkronreaktans

$$X_{s,u} = \frac{E_{af}(I_f)}{I_{a,sc}(I_f)} = \left/ \frac{V_{ag}(\hat{I}_f)}{\hat{I}_{a,sc}(\hat{I}_f)} \right/ = \frac{V_{ag}(\hat{I}_f)}{\hat{I}_{a,sc}(\hat{I}_f)}$$

De motorn är omätnad  
gäller att  
 $X_{s,u} = \frac{V_{ag}(I_f)}{I_{a,sc}(I_f)}$ , för alla  $I_f$

Mätnad synkronreaktans

$$X_s = \frac{E_{af}(I_f)}{I_{a,sc}(I_f)} = \left/ \frac{V_{rated}}{\bar{I}_{a,sc}} \right/ = \frac{V_{rated}}{\bar{I}_{a,sc}}$$

Ex 45 kVA, 220V, 3-fas, 60 Hz synkronmotor ⑦

$f_c = 60 \text{ Hz}$	Prov 1 (omättad)	Prov 2 (mättad)
$I_f \text{ [A]}$	2,2	2,84 $\leftarrow \bar{I}_f$
oc $V_{a,l-l} \text{ [V]}$	—	<span style="border: 1px solid black; padding: 2px;">220</span> $\leftarrow$ märkspänning
oc $V_{a,ag,4} \text{ [V]}$	202	—
sc $I_a \text{ [A]}$	<span style="border: 1px solid black; padding: 2px;">118</span> märkström	152 $\leftarrow \bar{I}_{a,sc}$

Sökt:  $X_{s,a}, X_s$   $\swarrow V_{a,ag,L-n} = \frac{V_{a,ag,L-L}}{\sqrt{3}}$

$$X_{s,a} = \frac{V_{a,ag}(I_f)}{\bar{I}_{a,sc}(I_f)} = \frac{202/\sqrt{3}}{118} = 0,99 \Omega/\text{fas}$$

$$X_s = \frac{V_{a,rated}}{\bar{I}_f} = \frac{220/\sqrt{3}}{152} = 0,84 \Omega/\text{fas}$$