## Försättsblad till skriftlig tentamen vid Linköpings Universitet

| Datum för tentamen | $2023-10-20$ |
| :--- | :--- |
| Sal | TER1, TERD, TERF |
| Tid | $14-18$ |
| Kurskod | TSTE25 |
| Provkod | TEN1 |
| Kursnamn | Effektelektronik (Power Eectronics) |
| Institution | ISY |
| Antal uppgifter som ingår i ten- <br> tamen | 5 |
| Antal sidor på tentamen <br> (inkl. försättsbladet) | 5 |
| Jour/kursansvarig | Lars Eriksson |
| Telefon under skrivtid | $079-061$ 20 73 (Arvind) |
| Besöker salen ca. | 15 och 17 |
| Tillåtna hjälpmedel | Vetenskaplig räknare, miniräknare, <br> 1 A4 medformler och information |
| Övrigt | Betygsgränser: <br> 20 poäng $=$ godkänd |

1. (a) (1 point) Draw the ideal characteristics for the Diode.
(b) (2 points) Draw the MOSFET drain current and the drain-to-source voltage when a positive pulse voltage is applied across the gate-source terminal.
(c) (2 points) When are the ideal characteristics used, and when are the more complicated characteristics (non-ideal) used?
2. The switched dc-dc step-down converter shown in Figure 1 controls a dc machine with an armature inductance $L_{\mathrm{a}}=0.2 \mathrm{mH}$. The armature resistance can be neglected. The armature current $i_{o}$ is 5 A . The switching frequency $f_{\text {sw }}=30 \mathrm{kHz}$ and the duty cycle, $D=0.8$. Consider all the components to be ideal.


Figur 1: Step-down DC-DC converter.
(a) (1 point) The output voltage, $V_{o}=200 \mathrm{~V}$. Calculate the input voltage, $V_{\mathrm{d}}$.
(b) (2 points) Find the ripple in the armature current.
(c) (2 points) Calculate the maximum and the minimum value of the armature current.
(d) (2 points) The load on the machine is reduced. Calculate $I_{\mathrm{a}}$ when the converter is on the boundary between continuous and discontinuous mode.
(e) (4 points) The load on the DC machine gives $I_{\mathrm{a}}=2 \mathrm{~A}$. Is the converter in discontinuous mode? Note: The duty-cycle of the converter is changed
3. An n-channel power MOSFET, a VMO 400-02F made by IXYS, is to be used in a converter ( $d a$ tasheet is attached). The MOSFET is to conduct a continuous current of 300 A when on and the switching frequency is 10 kHz with a $50 \%$ duty cycle. The input voltage is 100 V . The internal junction temperature is not to exceed $100^{\circ} \mathrm{C}$ and the maximum ambient temperature is $35^{\circ} \mathrm{C}$.
(a) (5 points) Calculate the total MOSFET power losses (assume the same time for voltage and current transients, i.e., $t_{\mathrm{ri}}=t_{\mathrm{fv}}=t_{\mathrm{r}}$ and $t_{\mathrm{fi}}=t_{\mathrm{rv}}=t_{\mathrm{f}}$ ).
(b) (2 points) Specify the thermal resistance of the required heat sink (Assume that the MOSTFET has no heat transfer paste).
(c) (2 points) Determine the peak MOSFET drain-to-source voltage during the switching transient if the blocking voltage (MOSFET drain-to-source voltage when it is completely turned off) is 100 V and the parasitic inductance is 100 nH .
4. The output voltages and current of a singe-phase full-bridge inverter are shown in the figure. Determine the following:
(a) (1 point) Type of modulation (unipolar or bipolar).
(b) (2 points) Switching frequency.
(c) (3 points) Inductance.
(d) (2 points) Peak fundamental current.
(e) (2 points) Pole-to-pole DC-link voltage $\left(V_{d}\right)$ and modulation index $\left(m_{a}\right)$.
(f) (2 points) Active power on the load at the fundamental frequency.
(g) (1 point) Phase angle of the fundamental current with respect to the inverter side voltage.
(h) (2 points) Active and reactive power on the converter at the fundamental frequency.


Figur 2: Single-phase DC to AC full-bridge inverter output waveforms.
5. The problem with ripple in the output current from a single-phase full bridge converter is to be studied. The first harmonic of the output voltage is given by $V_{\mathrm{o}(1)}$ at $f_{1}=50 \mathrm{~Hz}$. The load is given in the figure as $L=10 \mathrm{mH}$ in series with an ideal voltage source $e_{\mathrm{o}}(t)$. It is assumed that the converter operates in sinusoidal PWM mode, bipolar modulation.

$$
e_{\mathrm{o}}(t)=\sqrt{2} 220 \sin \left(2 \pi f_{1} t\right)
$$

(a) (1 point) The frequency of the triangular signal is 1050 Hz . Calculate the frequency modulation ratio (or pulse number), $m_{f}$.
(b) (1 point) Find the dc-voltage when the converter fundamental RMS output voltage $V_{o(1)}$ is 230 V and modulation index, $m_{a}=0.6$.
(c) (2 points) Determine the RMS fundamental output current (i.e., current through the inductor).
(d) (3 points) Determine the RMS and frequency of the highest output ripple current component.
(e) (3 points) If a Unipolar modulation is used, determine the RMS and frequency of the highest output ripple current component.
Note: Ripple here is referred to as distortion, which is the alteration of the original shape of a signal. Here ripple means the alteration of the waveform from an ideal sinusoidal signal.

Tabell 1: Generalized harmonics of a half-bridge inverter output voltage for a large $m_{f}$.

| $h \downarrow m_{a} \rightarrow$ | 0.2 | 0.4 | 0.6 | 0.8 | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0.2 | 0.4 | 0.6 | 0.8 | 1 |
| Fundamental |  |  |  |  |  |
| $m_{f}$ | 1.242 | 1.15 | 1.006 | 0.818 | 0.6023 |
| $m_{f} \pm 2$ | 0.061 | 0.061 | 0.131 | 0.22 | 0.318 |
| $m_{f} \pm 4$ |  |  |  |  | 0.018 |
| $2 m_{f} \pm 1$ | 0.19 | 0.326 | 0.37 | 0.314 | 0.181 |
| $2 m_{f} \pm 3$ |  | 0.024 | 0.071 | 0.139 | 0.212 |
| $2 m_{f} \pm 5$ |  |  |  | 0.013 | 0.033 |
| $3 m_{f}$ | 0.335 | 0.123 | 0.083 | 0.171 | 0.133 |
| $3 m_{f} \pm 2$ | 0.044 | 0.139 | 0.203 | 0.176 | 0.062 |
| $3 m_{f} \pm 4$ |  | 0.012 | 0.047 | 0.104 | 0.157 |
| $3 m_{f} \pm 6$ |  |  |  | 0.016 | 0.044 |
| $4 m_{f} \pm 1$ | 0.163 | 0.157 | 0.088 | 0.105 | 0.068 |
| $4 m_{f} \pm 3$ | 0.012 | 0.070 | 0.132 | 0.115 | 0.009 |
| $4 m_{f} \pm 5$ |  |  | 0.034 | 0.084 | 0.119 |
| $4 m_{f} \pm 7$ |  |  |  | 0.017 | 0.05 |

Note: output voltage $\left(\hat{V}_{o}\right)$ is $\hat{V}_{o}=m_{a} V_{d} / 2$.

$\boxed{\square X X S} \quad$ VMO 400-02F

| Symbol | Test Conditions <br> Characteristic Values ( $\mathrm{T}_{\mathrm{J}}=25^{\circ} \mathrm{C}$, unless otherwise specified) |  |  | Dimensions in mm ( $1 \mathrm{~mm}=0.0394$ ) |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| $\mathrm{g}_{\text {ts }}$ | $V_{D S}=10 \mathrm{~V} ; \mathrm{I}_{\mathrm{D}}=0.5 \cdot \mathrm{I}_{\mathrm{D} 25}$ pulsed | 380 | S |  |
| $\mathrm{C}_{\text {iss }}$ | \} $V_{G S}=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{DS}}=25 \mathrm{~V}, \mathrm{f}=1 \mathrm{MHz}$ | 53 | nF |  |
| $\mathrm{C}_{\text {oss }}$ |  | 9.6 | nF |  |
| $\mathrm{C}_{\text {rss }}$ |  | 3.4 | nF | $\square\|\mid 10$ |
| $\mathrm{t}_{\mathrm{d}(0 n)}$ | $\mathrm{V}_{G S}=10 \mathrm{~V}, \mathrm{~V}_{\mathrm{DS}}=0.5 \cdot \mathrm{~V}_{\text {DSS }}, \mathrm{I}_{\mathrm{D}}=0.5 \cdot \mathrm{I}_{\text {D25 }}$$\mathrm{R}_{\mathrm{G}}=1 \Omega$ (External) | 210 | ns |  |
| $\mathrm{t}_{\mathrm{r}}$ |  | 500 | ns | , $0^{2} 0^{2}$ 3 0 |
| $\mathrm{t}_{\text {d(off) }}$ |  | 900 | ns |  |
| $\mathrm{t}_{\text {f }}$ |  | 350 | ns | $\xrightarrow[74.5]{-46,5})^{85}$ |
| $Q_{g}$ | $\mathrm{V}_{\mathrm{GS}}=10 \mathrm{~V}, \mathrm{~V}_{\mathrm{DS}}=0.5 \cdot \mathrm{~V}_{\text {DSS }}, \mathrm{I}_{\mathrm{D}}=0.5 \cdot \mathrm{I}_{\mathrm{D} 25}$ | 2300 | nC | $\cdots$ |
| $Q_{\text {gs }}$ |  | 420 | nC |  |
| $Q_{\text {gd }}$ |  | 1150 | nC |  |
| $\mathrm{R}_{\text {thJc }}$ | with $30 \mu \mathrm{~m}$ heat transfer paste |  | 0.051 K/W |  |
| $\mathbf{R}_{\text {thJk }}$ |  |  | 0.076 K/W |  |


| Source-Drain Diode $\quad\left(\mathrm{T}_{\mathrm{J}}=25^{\circ} \mathrm{C}\right.$, |  | Characteristic Values ess otherwise specified) |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Symbol | Test Conditions | min. ${ }^{\text {typ. }}$ | max. |  |
| $\mathrm{I}_{\mathrm{s}}$ | $\mathrm{V}_{\text {GS }}=0 \mathrm{~V}$ |  | 418 | A |
| $\mathrm{I}_{\text {sm }}$ | Repetitive; pulse width limited by $\mathrm{T}_{\mathrm{JM}}$ |  | 1672 | A |
| $\mathrm{V}_{\text {sD }}$ | $\begin{aligned} & I_{F}=I_{s} ; V_{G S}=0 \mathrm{~V}, \\ & \text { Pulse test, } t \leq 300 \mu \mathrm{~s} \text {, duty cycle } \mathrm{d} \leq 2 \% \end{aligned}$ | 0.9 | 1.2 | V |
| $\mathrm{t}_{\mathrm{r}}$ | $\mathrm{I}_{\mathrm{F}}=\mathrm{I}_{\mathrm{S}},-\mathrm{di} / \mathrm{dt}=1200 \mathrm{~A} / \mu \mathrm{s}, \mathrm{V}_{\mathrm{DS}}=100 \mathrm{~V}$ | 600 |  | ns |

[^0]
[^0]:    IXYS MOSFETS and IGBTs are covered by one or more of the following U.S. patents:
    $4,835,5924,881,106 \quad 5,017,508 \quad 5,049,961 \quad 5,187,1175,486,715$
    $4,850,072 \quad 4,931,844 \quad 5,034,796 \quad 5,063,307 \quad 5,237,4815,381,025$

